

(19)



Europäisches Patentamt  
European Patent Office  
Office européen des brevets

(11) Publication number:

**0 370 618  
A1**

(12)

## EUROPEAN PATENT APPLICATION

(21) Application number: **89310729.2**

(51) Int. Cl.<sup>5</sup>: **B22F 7/00, A61F 2/30**

(22) Date of filing: **18.10.89**

The title of the invention has been amended  
(Guidelines for Examination in the EPO, A-III,  
7.3).

(30) Priority: **03.11.88 GB 8825723**

(43) Date of publication of application:  
**30.05.90 Bulletin 90/22**

(84) Designated Contracting States:  
**AT BE CH DE ES FR GB GR IT LI LU NL SE**

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(54) **Coated metallic prosthetic component.**

(57) A method of applying a porous metallic coating to the surface of a metallic prosthetic component such as an artificial limb, comprises the steps of forming a slurry comprising a suspension of particulate material in a solution of water containing a film-forming binder material, applying to the component or a part thereof a coating of the slurry, applying heat to the coating to gel the film-forming binder and to dry the slurry coating, and sintering the component to bond the particulate material onto the surface of the component.

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### Improvements in the Production of Coated Components

A method of applying a fully alloyed porous metallic coating to the surface of a metallic prosthetic component comprises the steps of producing a slurry comprising a suspension of the alloy in particulate form in a solution of water containing a film-forming binder material, applying to one or more surfaces of the component a coating of the slurry, heating the slurry coating to dry the same, and sintering the coated component to bond the particulate alloy onto the surface of the component.

This invention relates to the production of coated metallic prosthetic components including orthopaedic implants.

Metallic prosthetic and orthopaedic components have been used for some considerable time for such purposes as joint reconstruction or replacement and fracture fixation. These components have been produced from a number of alloys having the required properties of biocompatibility, strength, corrosion resistance and wear resistance. In addition, prosthetic components have hitherto been provided with a porous surface for enhanced fixation.

The production of such components especially those components having porous fully alloyed surfaces, is both time consuming and expensive. Indeed, no entirely satisfactory method of producing prosthetic components having a porous alloyed surface of uniform thickness and properties has been found.

The present invention sets out to provide a method of applying a porous fully alloyed surface to one or more selected areas of a prosthetic component, for example an orthopaedic component, which at least alleviates many of the problems and disadvantages previously encountered.

According to the present invention in one aspect there is provided a method of applying a fully alloyed porous metallic coating to the surface of a metallic prosthetic component, the method comprising the steps of producing a slurry comprising a suspension of the alloy in particulate form in a solution of water containing a film forming binder material, applying to one or more surfaces of the component a coating of the slurry, heating the slurry coating to dry the same, and sintering the coated component to bond the particulate alloy onto the surface of the component.

The slurry coating may be applied to the component by immersing the member wholly or partially in slurry. Alternatively, the slurry may be sprayed onto the surface of the component (or a part thereof) or a cloth or mesh (e.g. a metallic mesh) impregnated with the slurry may be wrapped around the component surface.

In an alternative arrangement, the slurry is injected into a mould positioned around the component surface, the spacing between the mould and the component determining the initial thickness of the slurry coating.

The applied coating may be subjected to an initial heating step to gel the film-forming binder and to a second heating step to dry the slurry. The initial heating step may be achieved by pre-heating the component to a temperature at which the film-forming binder gels on application of the slurry coating onto the heated component surface. Alternatively, the heating step may effect both gelling and drying of the binder.

The surface of the component may be roughened initially to provide enhanced bonding for the slurry coating. This may be achieved by applying a relatively thin, initial powder coating to the component and then sintering the powder coating to bond the same onto the surface of the component.

Preferably the particulate material is a fully alloyed metallic powder of mean particle size up to 250 microns. The mean particle size of the powder may lie within the range 30-150 microns. The film-forming binder may comprise methyl cellulose, the viscosity of the slurry then preferably lying within the range 5000-25000 centipoises.

The particulate material may be produced by a gas atomisation technique or by any other suitable technique, e.g. chemical or water atomisation.

The alloy is preferably a cobalt based alloy which includes chromium and molybdenum.

After gelling of the slurry and before sintering, depressions may be formed in the coating to promote fixation of the orthopaedic component when in use. The depressions are preferably generally concave and re-entrant. The depressions may be formed by pressing heat degradable spheres into the gelled coating, the spheres burning off during the subsequent drying or sintering process.

According to the present invention in a further aspect there is provided a prosthetic orthopaedic component on which is formed a porous coating of a fully alloyed metallic material, the coating having been applied by one of the methods described in the preceding ten paragraphs.

The invention will now be described with reference to the following Example of a method of applying to an orthopaedic component, a porous fully alloyed coating which, in use, provides enhanced fixation.

A slurry is produced comprising a suspension of metallic powder of notional composition by weight: 27% Cr; 0.25% C; 5% Mo; 2.8% Ni; bal-

ance Co in a solution of water containing a film-forming binder material (such as methyl cellulose). A coating of this slurry is applied to a circumferential surface of a prosthetic orthopaedic component, e.g. a primary femoral component, of composition similar to that of the powder. The coating is applied to the proximal region of the component for enhanced fixation of the component in use.

Typically, the mean particle size of the metallic powder is less than 250 microns, preferably between 10 and 100 microns, for example 50 microns, and the viscosity of the slurry typically lies within the range of five thousand to twenty five thousand centipoises.

Slurries having viscosities outside of this range may, however, be used. Thus, if a non-gelling binder such as sodium carboxy methyl cellulose is employed, the viscosity of the slurry will be in excess of twenty five thousand centipoises.

The slurry coating may be applied to the surface of the component in any one of several ways. Thus, the component may be partially immersed in the slurry; alternatively, the slurry may be sprayed onto the component surface of may be applied by a suitably shaped blade or with a brush. Alternatively, particularly when an even coating of a predetermined thickness is required, the surface area of the component to be coated may be encased by a mould, the slurry being injected under pressure into the space defined between the component surface and the mould.

Typically, the thickness of the applied coating will be of the order of between 1mm and 5mm.

The coated component is heated at a temperature of around 50°C to gel the methyl cellulose binder. It is then further heated to a temperature of the order of 110°C to dry the slurry coating.

Gelling may be achieved by preheating the component to a temperature (e.g 60°C) at which on application of the slurry, gelling of the binder content of the slurry occurs. Where the coating is applied by an injection moulding technique, the heat may be applied to the slurry via the mould walls.

Heat degradable spheres, e.g. of polystyrene, are pressed into the gelled coating to a depth just greater than their central planes, the coating then closing partially over the exposed sphere surfaces.

The coated component is thereafter sintered in a sinter furnace at a temperature of between 1000°C and 1500°C to bond the metal powder to the surface of the metallic member. The sintering temperature is to a significant extent dependent upon the porosity of the coating required for the product. Thus, increases in sintering temperature produce a less porous coating.

During the drying or sintering stages the heat degradable spheres burn off to leave re-entrant

generally concave depressions in the component surface. These depressions assist fixation of the component in use. If an impregnated cloth has been used to apply the coating to the member, this cloth will also burn off during sintering. If a metallic mesh is employed, then the mesh itself may form part of the final coating.

Where the slurry coating is applied by an injection moulding technique the inner mould wall may be formed with convex protrusions which produce in the gelled coating the required concave re-entrant depressions.

It is to be understood that the foregoing is merely exemplary of the invention and that modifications can readily be made thereto without departing from the true scope of the invention. Thus, the particulate material may be of any suitable material, e.g copper or copper alloys for bearing applications; in such cases the temperatures referred to above will vary. Further, in order to achieve enhanced bonding, the surface of the component may be roughened prior to coating. This may, for example, be achieved by applying an initial relatively thin powder coating to the component.

#### Claims

30 1. A method of applying a fully alloyed porous metallic coating to a surface of a metallic component in which the coating is produced from a slurry which comprises a suspension of the alloy in particulate form in a solution of water containing a film-forming binder material, the method being characterised in that the slurry is applied to one or more surfaces of a metallic prosthetic component, is heated to dry the same and is subsequently sintered to bond the particulate alloy content of the coating onto the respective surface of the component.

45 2. A method as claimed in Claim 1 or Claim 2 characterised in that the slurry is injected into a mould positioned around that or those component surfaces to be coated, the spacing between the mould and the component determining the initial thickness of the slurry coating.

50 3. A method as claimed in Claim 1 or Claim 2 characterised in that the applied coating is subjected to an initial heating step to gel the film-forming binder and to a second heating step to dry the slurry.

55 4. A method as claimed in Claim 3 characterised in that the initial heating step is achieved by pre-heating the component to a temperature at which the film-forming binder gels on application of the slurry coating onto the heated component surface.

5. A method as claimed in any one of the preceding claims characterised in that a relatively thin, initial powder coating is applied to a surface of the component, this coating subsequently being sintered to bond the coating onto the surface of the component to roughen the same. 5

6. A method as claimed in any one of the preceding claims characterised in that the particulate material is a fully alloyed metallic powder of mean particle size no greater than 250 microns. 10

7. A method as claimed in any one of the preceding claims characterised in that the alloy is a cobalt based alloy which includes chromium and molybdenum.

8. A method as claimed in any one of the preceding claims characterised in that, prior to sintering, generally concave and re-entrant depressions are formed in the coating to promote fixing of the component when in use. 15

9. A method as claimed in Claim 8 characterised in that the depressions are formed by pressing heat degradable spheres into the gelled coating, the spheres burning off during the subsequent drying or sintering process. 20

10. A prosthetic component on which is formed a porous coating of a fully alloyed metallic material, the coating having been applied by a method as claimed in any one of the preceding claims. 25

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# EUROPEAN SEARCH REPORT

Application Number

EP 89 31 0729

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
X	WO-A-8 300 282 (BATTELLE) * Claims 1,3-7,11,13 * ---	1-10	B 22 F 7/00 A 61 F 2/30
A	US-A-4 612 160 (A.L. DONLEVY et al.) * Claim 1 * -----	1-10	
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			B 22 F A 61 F
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 05-02-1990	Examiner SCHRUIERS H.J.
<b>CATEGORY OF CITED DOCUMENTS</b> X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			